

Lecture 6

Monday, April 18, 2005

Supplementary Reading: Osher and Fedkiw, §14.3.2, §14.3.3

In the previous lecture we introduced the numerical flux function. To review, we start with the strong form of the conservation law,

$$u_t + f(u)_x = 0.$$

Integrating over a grid cell, we have the weak form

$$(u_{ave,i}\Delta x)_t + f\left(u_{i+\frac{1}{2}}\right) - f\left(u_{i-\frac{1}{2}}\right) = 0.$$

Replacing $u_{ave,i}$ with the pointwise value u_i we make an $O(\Delta x^2)$ error

$$(u_i\Delta x)_t + f\left(u_{i+\frac{1}{2}}\right) - f\left(u_{i-\frac{1}{2}}\right) = O(\Delta x^2)$$

Introducing the numerical flux function instead of the physical flux function eliminates the error

$$(u_i)_t + \frac{\mathcal{F}\left(x_{i+\frac{1}{2}}\right) - \mathcal{F}\left(x_{i-\frac{1}{2}}\right)}{\Delta x} = 0.$$

1 Constructing the Numerical Flux Function

We define the numerical flux function through the relation

$$f(u_i)_x = \frac{\mathcal{F}_{i+1/2} - \mathcal{F}_{i-1/2}}{\Delta x} \tag{1}$$

To obtain a convenient algorithm for computing this numerical flux function, we define $h(x)$ implicitly through the following equation

$$f(u(x)) = \frac{1}{\Delta x} \int_{x-\Delta x/2}^{x+\Delta x/2} h(y)dy \tag{2}$$

and note that taking a derivative on both sides of this equation yields

$$f(u(x))_x = \frac{h(x + \Delta x/2) - h(x - \Delta x/2)}{\Delta x} \quad (3)$$

which shows that h is identical to the numerical flux function at the cell walls. That is $\mathcal{F}_{i\pm 1/2} = h(x_{i\pm 1/2})$ for all i . We calculate h by finding its primitive

$$H(x) = \int_{x_{-1/2}}^x h(y) dy \quad (4)$$

using polynomial interpolation, and then take a derivative to get h . We build a divided difference table to construct H .

<u>zeroth order</u>	$D_{i+\frac{1}{2}}^0 H$	at cell walls
<u>first order</u>	$D_i^1 H$	at cell centers
<u>second order</u>	$D_{i+\frac{1}{2}}^2 H$	at cell walls
<u>third order</u>	$D_i^3 H$	at cell centers
\vdots	\vdots	\vdots

That is, the even divided differences of H are at the cell walls, and the odd divided differences of H are at the cell centers. Since we are actually interested in determining h , we do not need the zeroth order divided differences of H as they will drop out when we differentiate to obtain h . Therefore, we can ignore the zeroth level of the divided difference table for H , and construct the table starting at the first level. The first level is given by

$$\begin{aligned} D_i^1 H &= \frac{H\left(x_{i+\frac{1}{2}}\right) - H\left(x_{i-\frac{1}{2}}\right)}{\Delta x} \\ &= f(u_i) \\ &= D_i^0 f \end{aligned}$$

This is because

$$\begin{aligned} H(x_{i+\frac{1}{2}}) &= \int_{x_{-1/2}}^{x_{i+1/2}} h(y) dy \\ &= \sum_{j=0}^i \left(\int_{x_{j-1/2}}^{x_{j+1/2}} h(y) dy \right) \\ &= \Delta x \sum_{j=0}^i f(u(x_j)) \end{aligned}$$

And similarly,

$$H(x_{i-\frac{1}{2}}) = \Delta x \sum_{j=0}^{i-1} f(u(x_j))$$

So that

$$H(x_{i+\frac{1}{2}}) - H(x_{i-\frac{1}{2}}) = \Delta x f(u(x_i))$$

The higher divided differences are

$$D_{i+1/2}^2 H = \frac{f(u(x_{i+1})) - f(u(x_i))}{2\Delta x} = \frac{1}{2} D_{i+1/2}^1 f \quad (5)$$

$$D_i^3 H = \frac{1}{3} D_i^2 f \quad (6)$$

continuing in that manner.

According to the rules of polynomial interpolation, we can take any path along the divided difference table to construct H , although they do not all give good results. ENO reconstruction consists of two important features. First, choose $D_i^1 H$ in the upwind direction. Second, choose higher order divided differences by taking the smaller in absolute value of the two possible choices. Once we construct $H(x)$, we evaluate $H'(x_{i+1/2})$ to get the numerical flux $\mathcal{F}_{i+1/2}$.

2 ENO-Roe Discretization (Third Order Accurate)

For a specific cell wall, located at $x_{i_0+1/2}$, we find the associated numerical flux function $\mathcal{F}_{i_0+1/2}$ as follows. First, we define a *characteristic speed*

$$\lambda_{i_0+1/2} = f'(u_{i_0+1/2})$$

For example, recall Burgers' equation,

$$u_t + \left(\frac{u^2}{2}\right)_x = 0.$$

The flux is given by

$$f(u) = \left(\frac{u^2}{2}\right)$$

so that

$$f'(u) = u$$

Therefore,

$$\lambda(x) = f'(u(x)) = u(x).$$

The value of u at the half grid points is defined using a standard linear average

$$u_{i_0+1/2} = (u_{i_0} + u_{i_0+1})/2$$

Then, if $\lambda_{i_0+1/2} > 0$, set $k = i_0$. Otherwise, set $k = i_0 + 1$. Define

$$Q_1(x) = (D_k^1 H)(x - x_{i_0+1/2}) \quad (7)$$

If $|D_{k-1/2}^2 H| \leq |D_{k+1/2}^2 H|$, then $c = D_{k-1/2}^2 H$ and $k^* = k - 1$. Otherwise, $c = D_{k+1/2}^2 H$ and $k^* = k$. Define

$$Q_2(x) = c(x - x_{k-1/2})(x - x_{k+1/2}) \quad (8)$$

If $|D_{k^*}^3 H| \leq |D_{k^*+1}^3 H|$, then $c^* = D_{k^*}^3 H$. Otherwise, $c^* = D_{k^*+1}^3 H$. Define

$$Q_3(x) = c^*(x - x_{k^*-1/2})(x - x_{k^*+1/2})(x - x_{k^*+3/2}) \quad (9)$$

Then

$$\mathcal{F}_{i_0+1/2} = H'(x_{i_0+1/2}) = Q_1'(x_{i_0+1/2}) + Q_2'(x_{i_0+1/2}) + Q_3'(x_{i_0+1/2}) \quad (10)$$

which simplifies to

$$\mathcal{F}_{i_0+1/2} = D_k^1 H + c(2(i_0 - k) + 1) \Delta x + c^* (3(i_0 - k^*)^2 - 1) (\Delta x)^2. \quad (11)$$